



## The Effect of Volatile Organic Compounds on GAC Adsorbers

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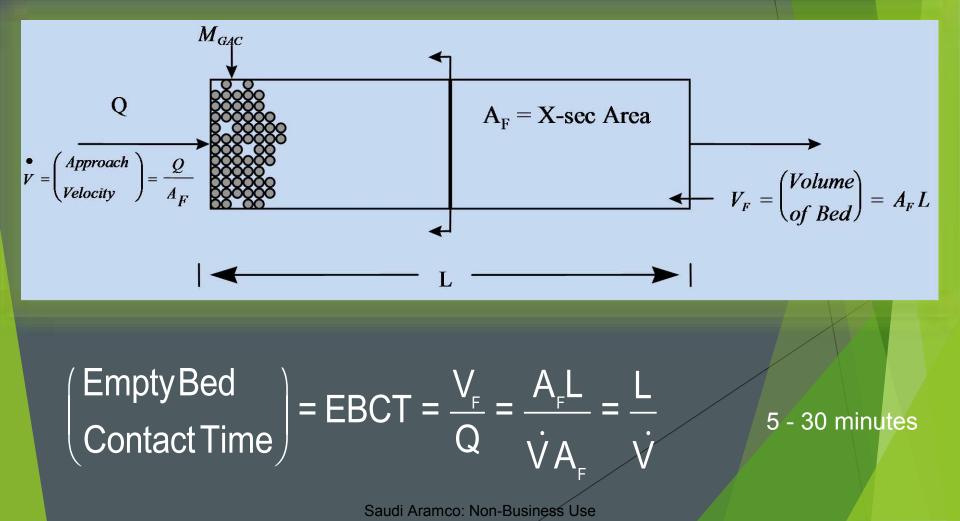
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## OUTLINE

- Important design parameters for fixed-bed adsorbers
- Methods for obtaining important design parameters
- Model predictions for a variety of VOCs & SOCs and water sources using the PSDM
- Analysis of VOC removal using GAC
- GAC costs for removal of VOCs.

## Important Variables in Fixed-bed Adsorption

GAC Adsorber size is quantified in terms of Empty Bed Contact Time.



## Important Variables in Fixed-bed Adsorption

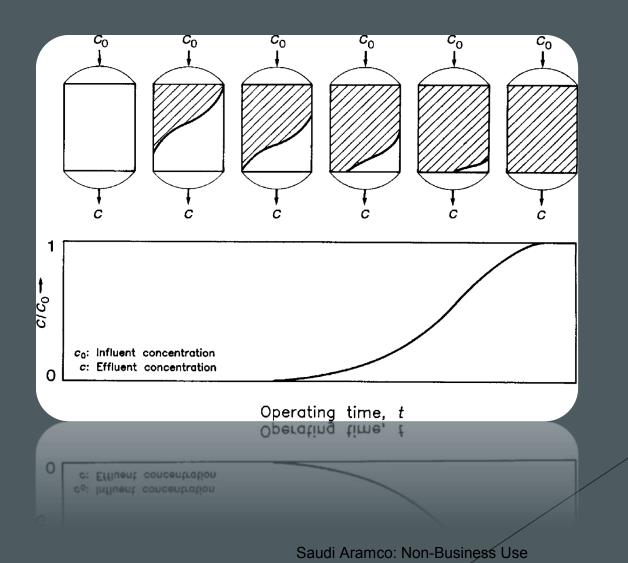
GAC Adsorber performance is quantified in terms of specific throughput. Defined as the volume fed to the adsorber divided by the mass of GAC in the adsorber.

$$\left( \begin{array}{c} \text{Specific} \\ \text{Throughput} \end{array} \right) = \frac{\text{Qt}}{\text{M}_{_{\text{GAC}}}}$$

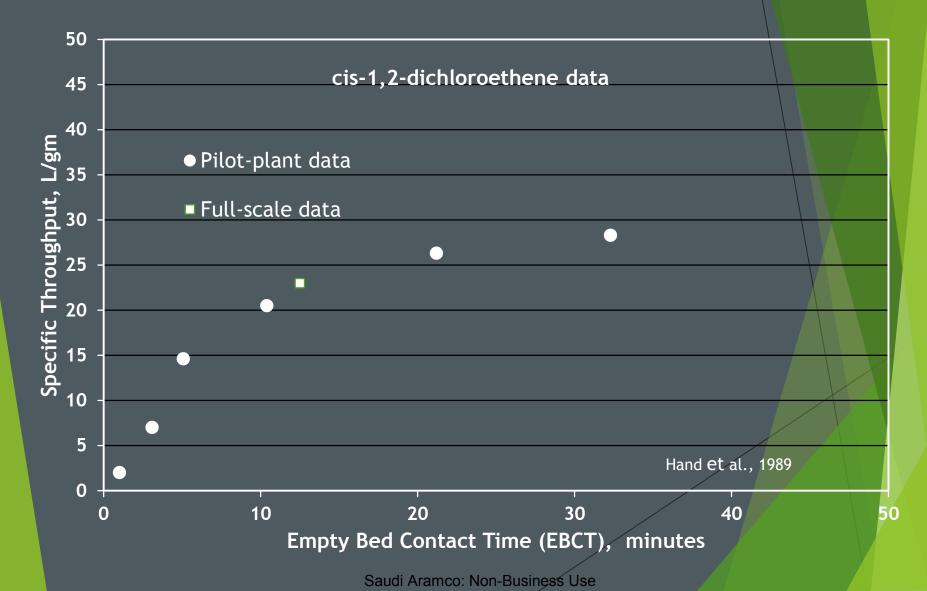
Another more common way to quantify the performance of a GAC adsorber is in terms of GAC usage rate.

$$\begin{pmatrix} GAC \\ UsageRate \end{pmatrix} = \frac{M_{GAC}}{Qt} = \frac{1}{\begin{cases} Specific \\ Throughput \end{cases}}$$

### Breakthrough Characteristics of Fixed-Bed GAC Adsorber



## Relationship Between Specific Throughput & EBCT



Full-Scale Studies Pilot-Plant Studies Rapid Small Scale Column Studies (RSSCTs) Mathematical Models

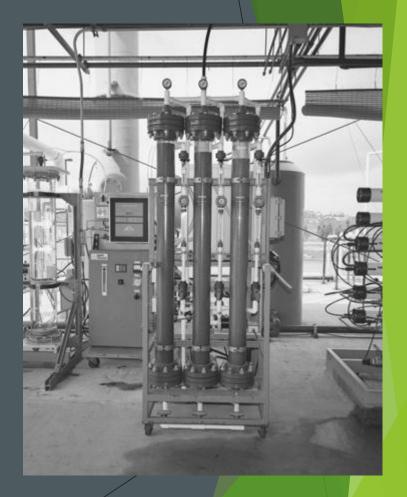
### **Full-Scale Studies:**

- Most effective method
- Most expensive
- Most time consuming



**Pilot Plant Studies:** 

- Effective method
- Expensive
- Time consuming



### **RSSCT Studies:**

Somewhat effective method
(Need scaling factor)
Cost can be reasonable
Short time (1 wk – 1 month)



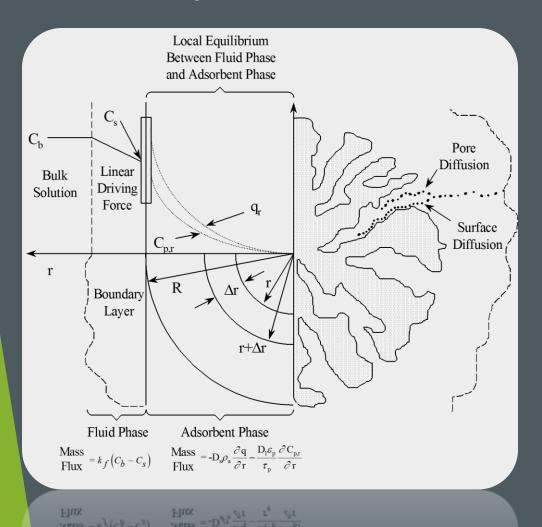
### **Mathematical Model:**

- Somewhat effective method
- Least Expensive
- Least Time Consuming



### Pore Surface Diffusion Model (PSDM)

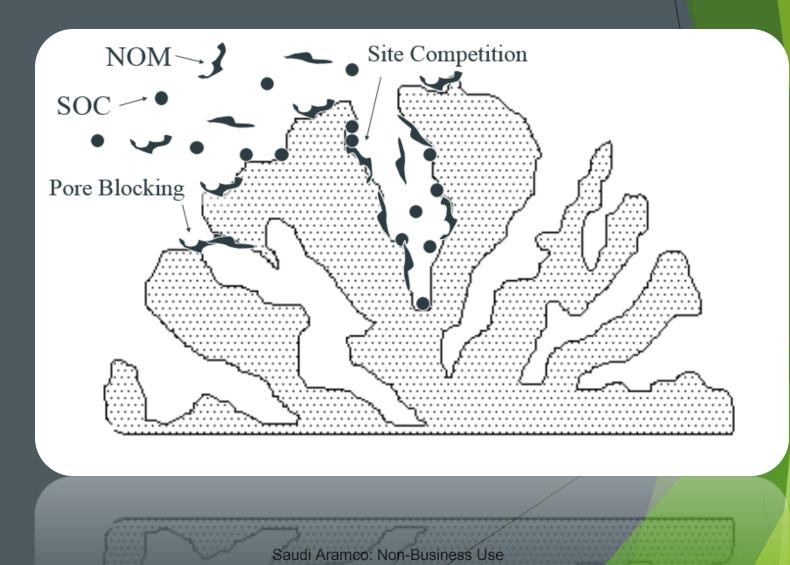
Schematic of Intraparticle Mass Transport Mechanisms:



Intraparticle Mass Transport Mechanisms & Assumptions:

- Diffusion resistance in the liquid-phase surrounding the adsorbent particles and may be described by a linear driving force approximation.
- Diffusion resistance within the adsorbent particle is described by Fick's law. Intraparticle mass transport is by both surface and pore diffusion.
- There is no channeling.
- Ideal Adsorbed Solution Theory (IAST) describes the competitive equilibrium.

### MECHANISMS of NOM Interference with VOC Adsorption



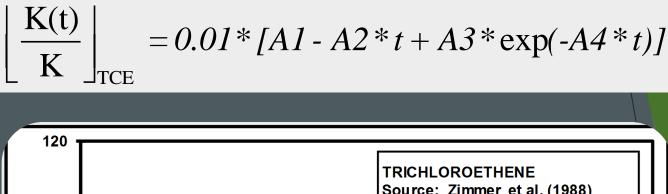
Model Parameters influenced by NOM Fouling

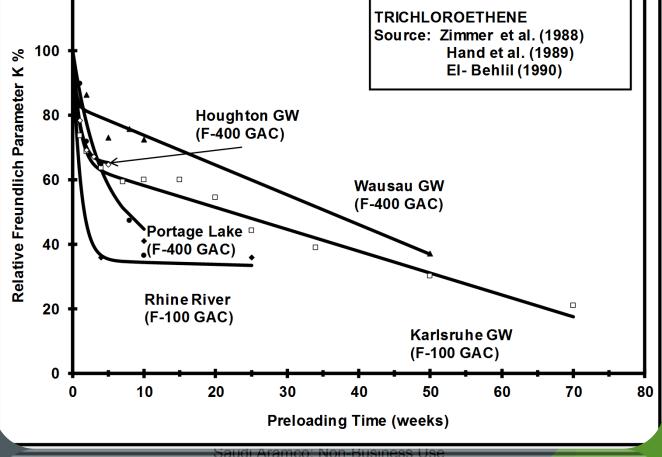
Freundlich Capacity Parameter, K

Surface Diffusion Coefficient: D<sub>s</sub>

Pore Diffusion Coefficient: D<sub>P</sub>

### Effect of Water Type (Background Matrix) (Sontheimer et al, 1988)





### Effect of Compound Type (Sontheimer et al, 1988)

$$\frac{\mathbf{K}(\mathbf{t})}{\mathbf{K}} = B_1 \times \left\lfloor \frac{\mathbf{K}(\mathbf{t})}{\mathbf{K}} \right\rfloor_{\mathrm{TCE}} + B_2$$

Correction Factors for the Reduction in Freundlich Isotherm Capacity Parameters for Different Classes of Compounds Relative to the Reference Compound of TCE

Class	Group	Surrogate Compound	B <sub>1</sub>	B <sub>2</sub>
	Halogenated Alkanes	1,1,1-Trichloroethane	1.2	-0.2
Purgeables	Halogenated Alkenes	Trichloroethene	1	0
	Trihalo- methanes	Chloroform	1	0
	Aromatics	Toluene	0.9	0.1
Base Neutrals	Nitro Compounds	3,4-Dinitrotoluene	0.75	0.25
	Chlorinated Hydrocarbons	1,4-Dichlorobenzene	0.59	0.41
Acids	Phenols	2,4-Dichlorophenol	0.65	0.35
Polynuclear- Aromatics (PNAs)		Methylene Blue	0.32	0.68
Pesticides		Atrazine	0	0.05

## Impact on Intraparticle Mass Transfer

- Surface Diffusion Coefficient becomes negligible
- Intraparticle Pore Diffusion Coefficient

$$D_p = \frac{D_l}{\tau_p}$$

– VOCs in the Presence of NOM:

- $\tau_p = 1.0$  when Time < 70 days
- $\tau_p = 0.334 + 6.61(10^{-6}) * t$  when Time > 70 days

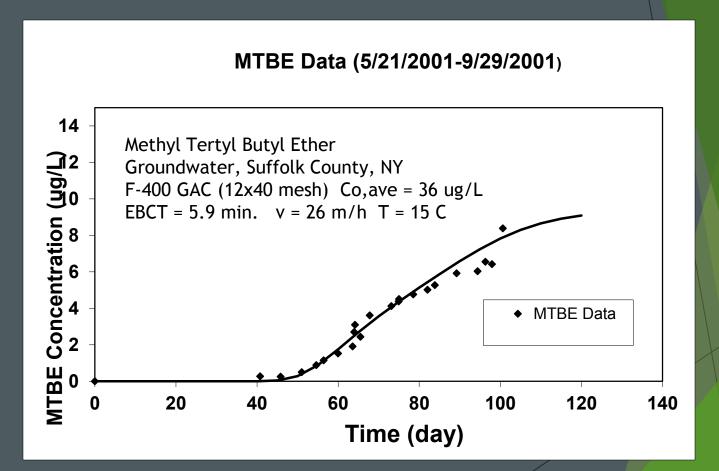
# Factors Influencing VOC Adsorption in the Presence of NOM

Preloading Time
Adsorbent type
Source Water
Solution chemistry
NOM molecular weight distribution
Solute Type

## MODEL VERIFICATION EFFORT

▶ 13 Case Studies 10 Pilot Plant Experiments ▶ 3 Full-Scale Plants ▶ 13 Water Sources ▶ 10 Groundwaters ▶ 3 Surface Waters ▶ 5 Adsorbents 50 Empty Bed Contact Times 16 Volatile & Synthetic Organic Chemicals

## MTBE: PSDM PREDICTION - KARLSRUHE TAP WATER CORRELATION

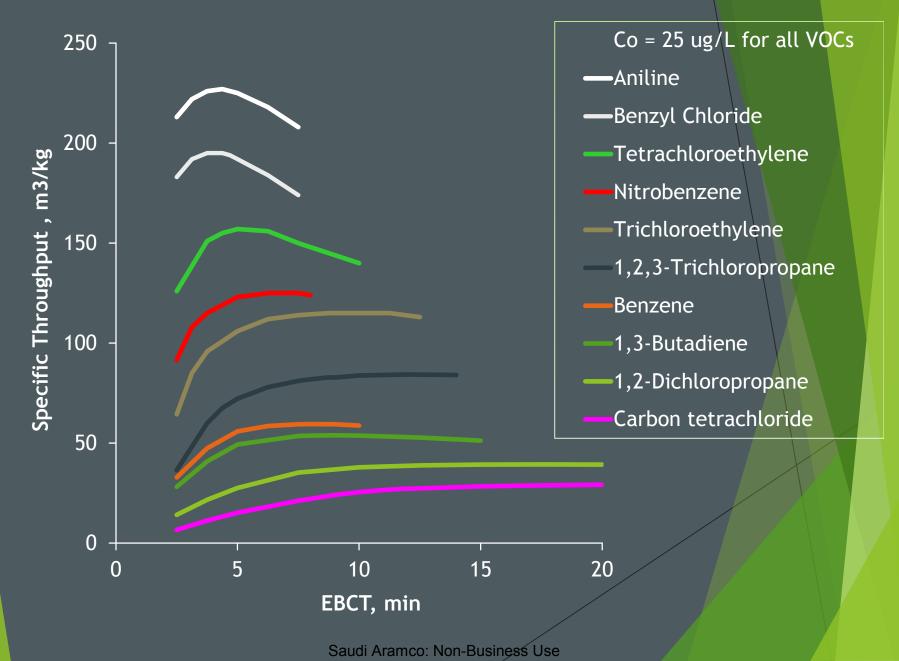


## Summary Table of VOCs and their Freundlich Isotherm Parameters

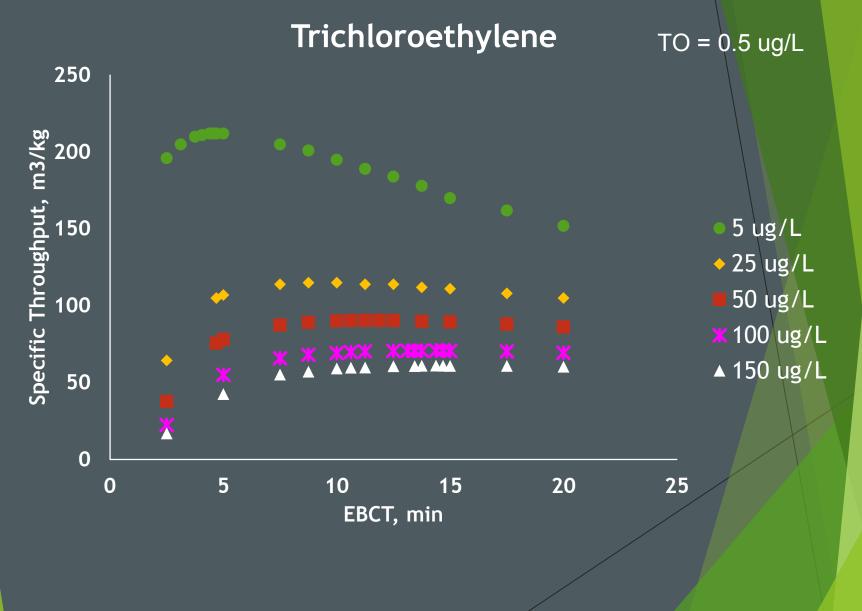
Compound	K(mg/g*(L/mg) <sup>1/n</sup> )	1/n	Source
aniline	63.4	0.2	Valderrama, 2010
benzyl chloride	144.42	0.346	Polanyi Estimation
tetrachloroethylene	245.6	0.458	Crittenden et al., 1985
nitrobenzene	61.67	0.417	Polanyi Estimation
trichloroethylene	60.1	0.416	Crittenden et al., 1987
1,2,3-trichloropropane	131.4	0.73	Speth et al., 1988
vinyl chloride	7.77	0.683	Polanyi Estimation
1,2-dichloroethane	11.8	0.832	Crittenden 1987
dichloromethane	2.339	0.79	Khan, 2010
urethane	1.46	0.581	Polanyi Estimation
oxirane, methyl	0.063	0.869	Polanyi Estimation

Calgon F400 carbon and isotherm temperature range 16 – 20 C

### Relationship between Specific Throughput and EBCT

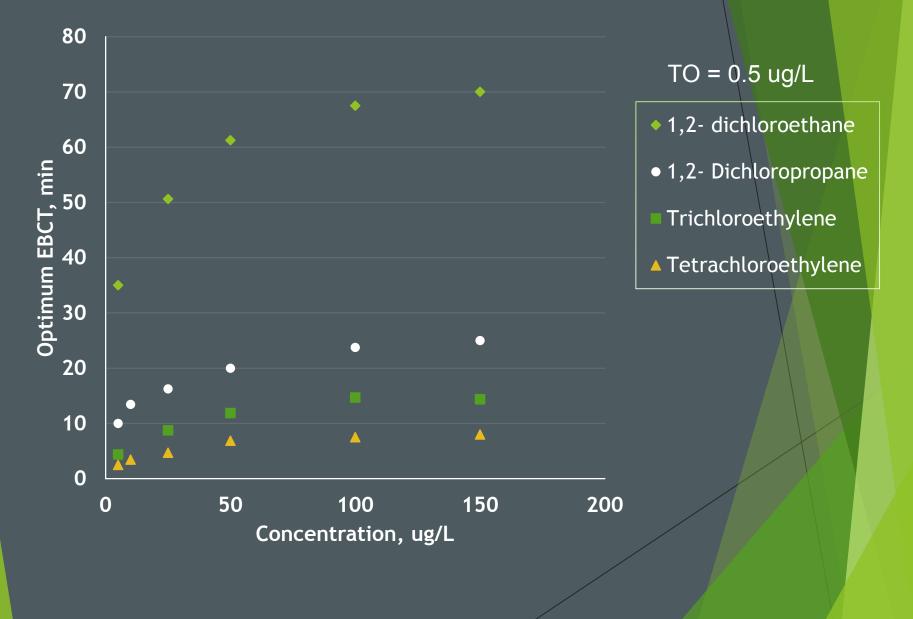


### Impact of Initial Concentration on Specific Throughput and EBCT

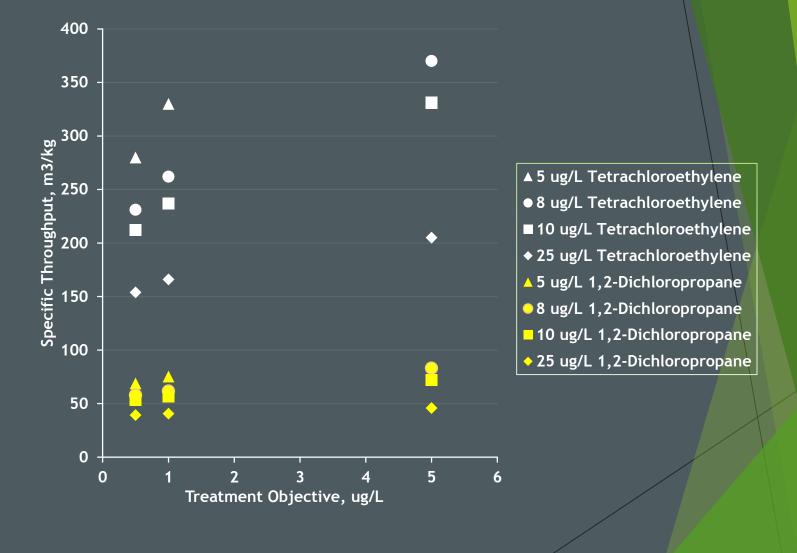


Saudi Aramco: Non-Business Use

### Relationship between Optimum EBCT and Initial Concentration



### Sensitivity of Specific Throughput to Treatment Objective



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Compound		% change in carbon usage rate			
Compound	Co, ug/L	TO 5 to 1 ug/L	TO 5 to .5 ug/L		
	25	19	25		
Tetrachloroethylene	10	28	36		
	8	29	38		
	25	11	14		
1,2-Dichloropropane	10	21	25		
	8	26	30		

TO = Treatment Objective

## Summary GAC Replacement Costs

	C <sub>o</sub>	Optimum	GAC Cost = \$/1000 gal		
Compound	μg/L	EBCT, min	MCL = 5	MCL = 1.0	MCL = 0.5
			μg/L	μg/L	μg/L
aniline	25	4.4	0.049	0.054	0.055
benzyl chloride	25	4.0	0.053	0.062	0.064
tetrachloroethylene	25	5.0	0.062	0.075	0.081
nitrobenzene	25	6.0	0.081	0.098	0.100
trichloroethylene	25	9.0	0.087	0.105	0.109
1,2,3-trichloropropane	25	12.0	0.113	0.139	0.148
Benzene	25	8.0	0.181	0.204	0 210
1,3-Butadiene	25	9.0	0.199	0.224	1 232
1,2- dichloropropane	25	18.0	0.275	0.308	0318
Carbon tetrachloride	25	25	0.362	0.412	0.1.16
vinyl chloride	25	25	0.944	1.001	1.018
1,2-dichloroethane	25	50	0.957	1.078	1.117
dichloromethane	25	80	3.355	3.466	3.495

#### Unit GAC cost = \$ 1.50 per lb

### Typical GAC Capital Costs

Configuration	Single bed	Beds in series
Design Flow, gpm	511	511
Vessel Diameter, ft	12	2 x 12
Site demolition, clearing and grubbing, \$	50,000	50,000
Purchase and install GAC vessel(s), \$	150,000	300,000
At-grade vessel foundation, \$	21,000	27,000
Site piping modifications/additions, \$	62,500	125,000
Electrical, metering, and telemetry modifications, \$	50,000	75,000
Backwash reclaim tank, foundation, and reclaim pump, \$	41,500	50,000
Miscellaneous site work, paving, vaults, walls, landscaping, \$	132,000	145,000
Mobilization @ 2 %, \$	10,140	15,440
Subtotal, \$	517,140	787,440
Contingencies @ 20%, \$	103,430	157490
Subtotal, \$	620,570	944,930
Engineering design, \$	125,000	150,000
Construction management and inspection, \$	59,000	65,000
Environmental/legal/ administration, \$	25,000	25,000
DPH operations plan/permitting, \$	15,000	15,000
Total capital costs, \$	845,000	1,200,000

### **Typical Operation and Maintenance Assumptions**

ltem	Value
Power unit cost, \$/KWh	0.13
Overall Pump efficiency, %	70
General labor hours, hr/wk	3
Additional inspection & maintenance hr/wk	1
Sampling labor, hr/sample	0.25
Labor unit cost, \$/hr	122
Required lab & sampling, samples/2wk	2
GAC change out labor requirement, hr	8
VOC sampling cost, \$/sample	150
BACT/HPC sampling costs, \$/sample	35
Present worth discount rate, %	2.7
Carbon unit cost, \$/lb	1.5

## Summary of Present Worth Values

Co, ug/L	Compound	Configuration Type	Treatm 5	ent Objecti <sup>.</sup> 1	ve, ug/L 0.5
25	aniline	Single bed	1,322,000	1,335,000	1,337,000
25	benzyl chloride	Single bed	1,334,000	1,356,000	1,360,000
25	tetrachloroethylene	Single bed	1,353,000	1,386,000	1,399,000
25	tetrachloroethylene	2 beds in series	1,674,000	1,681,000	1,683,000
8	tetrachloroethylene	Single bed	1,333,000	1,386,000	1,410,000
25	nitrobenzene	Single bed	1,397,000	1,438,000	1,443,000
25	trichloroethylene	Single bed	1,409,000	1,453,000	1,462,000
25	1,2,3-trichloropropane	Single bed	1,469,000	1,532,000	1,554,000
25	Benzene	Single bed	1,636,000	1,692,000	1,706,000
25	1,3-Butadiene	Single bed	1,677,000	1,737,000	1,757,000
25	1,2- dichloropropane	Single bed	1,861,000	1,945,000	1,971,000
8	1,2- dichloropropane	Single bed	1,558,000	1,683,000	1,713,000
25	Carbon tetrachloride	Single bed	2,052,000	2,170,000	2,204,000
25	vinyl chloride	Single bed	3,420,000	3,555,000	3,595,000
25	1,2-dichloroethane	Single bed	3,441,000	3,723,000	3,815,000
25	dichloromethane	Single bed	9,036,000	9,296,000	9,364,000

## Summary

Models can be used to evaluate VOC fixed-bed adsorber performance.

- For a single adsorber the optimum EBCT will depend upon the VOC's adsorption potential and initial concentration.
  - VOCs with higher adsorption potentials require smaller EBCTs to maximize specific throughput.
  - Lower initial VOC concentrations require lower EBCTs to maximize specific throughput.
- Carbon usage rate is dependent upon the initial VOC concentration and treatment objective.
  - As initial VOC concentration decreases the carbon usage rate decreases for a given treatment objective.
  - As initial VOC concentration decreases the effect of lowering the treatment objective on carbon usage rate increases.

## Conclusions

For existing systems treating high initial VOC concentrations the impact of lowering the treatment objective is negligible.

For existing systems treating low initial VOC concentrations the impact of reducing the treatment objective becomes important.

For situations where VOC concentrations are at or just below current MCLs the capital cost is a major issue.

## Questions ?